

PCT

WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau



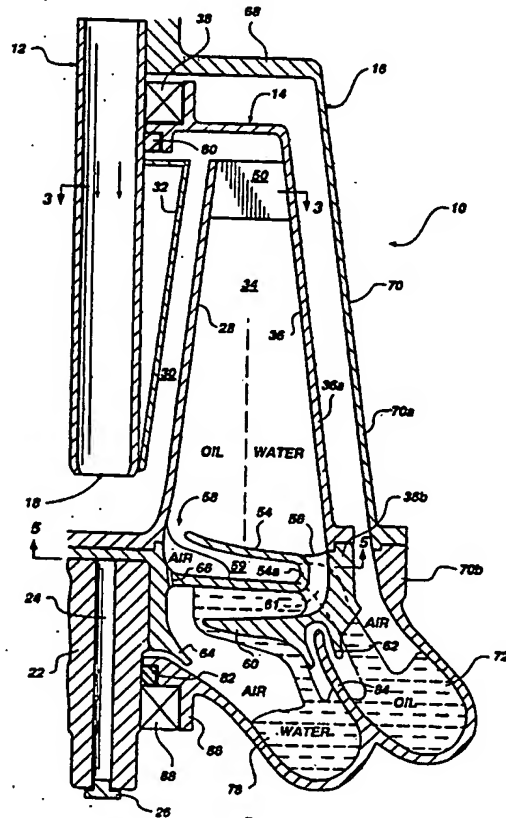
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁵ : B01D 21/26		A1	(11) International Publication Number: WO 93/25294 (43) International Publication Date: 23 December 1993 (23.12.93)
(21) International Application Number: PCT/US93/05505 (22) International Filing Date: 9 June 1993 (09.06.93) (30) Priority data: 07/896,185 10 June 1992 (10.06.92) US (71) Applicant: TAGGART, Charles, W. [US/US]; 234 Seventh Avenue, Salt Lake City, UT 84103 (US). (72) Inventor: ROGERS, Ernest ; 1735 Cherokee, Pleasant Grove, UT 84062 (US). (74) Agents: THORPE, Calvin, E. et al.; Thorpe, North & Western, 9035 South 700 East, Suite 200, Sandy, UT 84070 (US).		(81) Designated States: AT, AU, BB, BG, BR, CA, CH, CZ, DE, DK, ES, FI, GB, HU, JP, KP, KR, KZ, LK, LU, MG, MN, MW, NL, NO, NZ, PL, PT, RO, RU, SD, SE, SK, UA, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG). Published With international search report.	

(54) Title: APPARATUS AND METHOD FOR CENTRIFUGALLY SEPARATING A FLUID MIXTURE INTO ITS COMPONENT PARTS

(57) Abstract

An apparatus and method for centrifugally separating a mixture of liquids comprises a central inlet shaft (12), a surrounding rotor (14), and a housing shell (16). The mixture is injected into the rotor through the inlet shaft and the rotor separates the mixture in a radially sloped separation space containing a first weir (54), discharges the lighter liquid into the housing through a channel (61) through the weir and wall (36) of the separation chamber, and discharges the heavier liquid into the housing over a second weir (60). The inlet shaft may be built up to provide for efficient sheer mixing and a sieve may be provided in the separation chamber. A two-stage separator may be constructed by providing a second separation chamber radially outward of the first after mixing of a separated liquid with a solvent and providing suitable discharge ports.



BEST AVAILABLE COPY

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	FR	France	MR	Mauritania
AU	Australia	GA	Gabon	MW	Malawi
BB	Barbados	GB	United Kingdom	NL	Netherlands
BE	Belgium	GN	Guinea	NO	Norway
BF	Burkina Faso	GR	Greece	NZ	New Zealand
BG	Bulgaria	HU	Hungary	PL	Poland
BJ	Benin	IE	Ireland	PT	Portugal
BR	Brazil	IT	Italy	RO	Romania
CA	Canada	JP	Japan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SK	Slovak Republic
CI	Côte d'Ivoire	LK	Sri Lanka	SN	Senegal
CM	Cameroon	LI	Liechtenstein	SU	Soviet Union
CS	Czechoslovakia	LU	Luxembourg	TD	Chad
CZ	Czech Republic	MC	Monaco	TG	Togo
DE	Germany	MG	Madagascar	UA	Ukraine
DK	Denmark	ML	Mali	US	United States of America
ES	Spain	MN	Mongolia	VN	Viet Nam
FI	Finland				

5 APPARATUS AND METHOD FOR CENTRIFUGALLY
 SEPARATING A FLUID MIXTURE INTO ITS COMPONENT PARTS

FIELD OF THE INVENTION

 The present invention concerns separation
apparatuses and methods, and particularly those systems
10 that separate two or more mixed fluid components through
centrifugation.

BACKGROUND OF THE INVENTION

 Centrifugal systems of separation use centrifugal
15 force generated through rotation to separate fluid
components of differing densities. In many fundamental
aspects, these systems are used as a substitute for and
improvement on gravitational separation techniques and
devices, since the gravitational force and the force
20 exerted on a fluid through rotation (centrifugal) are
identical in that they increase in magnitude as the
fluid increases in mass. Those fluids with lesser
density will be less influenced by the force and
therefore less inclined toward the source of the force,
25 the earth for gravitational, the outside of the rotating
container for centrifugal, than fluids with greater
density. The fluids will thus separate out and can be
directed to separate collection ports by using weirs or
other suitable separating structures. Centrifugal
30 separation is often more desirable than gravitational
because the force applied to the fluid can be controlled
through rotation speed and can be made to be many times
that of gravity.

 A common example of fluid separation is that of oil
35 from water. There are many situations in which
separation of these two elements is desired, such as oil

spills on an ocean or lake, mixing of the two fluids in ships' bilges, gasoline spills, etc. This process is often important for maintenance of quality of life in a particular geographic area. These two fluids are susceptible to centrifugal separation because water is denser than oil and thus will "sink" relative to the other under application of centrifugal force. This can easily be understood by the fact that oil floats on water in a gravitational field. Other fluid separation applications include wine clarification, waste-water treatment, blood plasma separation, and the like. Centrifugation is also used to separate solids out of liquids through sedimentation.

It is often desirable to separate dissolved elements in solution or emulsion. Standard centrifugal separation equipment alone cannot carry out such a separation since the dissolved elements will move with the solution. A solvent must therefore be introduced into the fluid stream to extract the dissolved elements. Such a process requires that the solvent be thoroughly mixed with the fluid to extract all dissolved elements. The solvent and fluid are then separated through centrifugation. An example of this type of separation is solvent extraction and separation of transuranic elements from radioactive waste streams at nuclear processing plants.

Meikrantz, U.S. Patent 4,959,158, is an example of a typical centrifugal separator in the prior art. In that apparatus, the fluid to be separated is introduced into a space between an inner rotor and an outer stationary housing, where shear mixing of the fluid occurs. A large amount of power is required to maintain the speed of the rotor against the viscous drag of the shearing liquid which makes the apparatus energy inefficient. The power loss increases with angular velocity, limiting the rotor speed.

The rotor is an open top cylinder with the separating weirs at the top. Meikrantz uses the space between the rotor and its housing to introduce the oil-water mixture to be separated. Thus the bottom portion
5 of the space is filled with liquid during operation. The top portion of the space, where the liquids separate and transfer from the rotor to the housing, must contain air for proper operation. In this space, no seals can be made between the incoming liquid and the air because
10 of the large diameter of the interface; the drag would be unacceptable. This highly agitated air/liquid interface causes the fluid input into the rotor to mix with the air, reducing flow capacity and causing foaming with many substances such as detergents in motor oil.
15 This foaming dramatically reduces the effectiveness of the separator and further increases viscous drag. Meikrantz allows a second air-water interface to exist within the rotor, as a core of air forms radially inward from the first weir, at the center of the rotor.
20 Energetic flow of liquid through the separator causes surface waves to form on this interface, which further degrades the separation process. Additionally, the lighter separated liquid spreads along the full length of the rotor between the air core and the partially
25 defined liquid/liquid interface. This disperse unstable mass is difficult to collect over the relatively short first weir.

OBJECTS AND SUMMARY OF THE INVENTION

30 It is therefore an object of the present invention to overcome the shortcomings of the prior art.

It is a further object of the invention to input and mix the fluid to be separated without admitting air.

It is a further object of the invention to provide
35 a centrifugal separator which can be made to operate in any orientation.

It is a further object of the invention to minimize fluid motion and contact of fluid with air, and to minimize the power required to operate a separator while maximizing flow capacity.

5 It is a further object of the invention to optimize the weir structure in centrifugal separators so that the fluid will separate under a wide range of conditions, and to control air pressure over the weirs and remove formed gases.

10 It is a further object of the invention to utilize lipophyllic surfaces more effectively than in stationary separators, to provide means for controlling fluid motion in the rotor, and to allow for complete automatic draindown and flushing.

15 It is a further object of the invention to provide a two-stage separator using solvent extraction for separation both of immiscible materials and dissolved materials, removal of foams and emulsions, and to obviate the need for a secondary process.

20 In accordance with a first aspect of the invention, an apparatus for centrifugally separating into its component parts a mixture having immiscible component parts of a first liquid and a second liquid of differing densities, comprises an elongate inlet shaft having an
25 open receiving end for receiving mixture and an open discharge end through which the mixture is delivered into the apparatus, a rotor disposed substantially coaxially to and surrounding the inlet shaft and adapted for rotational movement thereabout, and a housing
30 surrounding the rotor for receiving and collecting the separated liquids from the rotor. The rotor contains a mixing chamber around the inlet shaft with walls comprising the inlet shaft itself and a frustoconical center wall surrounding the inlet shaft, a separation
35 chamber which receives the mixture from the mixing chamber whose inner wall is the frustoconical center wall and whose outer wall slopes oppositely the center

10 wall and a first weir disposed at the bottom of the separation chamber. A lighter liquid channel is formed between the base of the first weir and the center wall, and a heavier liquid channel is formed between the first
5 weir and the outer wall. A discharge passage for the lighter liquid is provided from the first weir to a collection chamber in the housing. A second weir is formed beneath the first weir for the discharge of the heavier liquid into a second collection chamber in the
10 housing.

15 In accordance with a second aspect of the invention, a method of centrifugally separating a mixture containing component parts of first and second immiscible liquids comprises the steps of inputting the
15 mixture through an input shaft into the approximate center of a rotatable rotor having a radially outwardly sloping center wall with an annular outer edge surrounding the input shaft, rotating the rotor causing the mixture to move down the slope of the center wall
20 and flow over the edge thereof into a separation chamber formed by the center wall and a coaxial outer wall having an opposite radial slope from the center wall and a first weir disposed oppositely from the center wall edge, separating the mixture into its component parts in
25 the separation chamber, discharging the first liquid from the separation chamber through a first annular channel between the center wall and the first weir, channeling the first liquid to a first collection chamber, discharging the second liquid from the
30 separation chamber through a second segmented annular channel between the outer wall and the base of the first weir, and channeling the second liquid to and over a second weir and into a second collection chamber.

35 In accordance with a third aspect of the invention, an apparatus for centrifugally separating into its component parts through solvent extraction a liquid mixture, containing first and second immiscible liquids

and contaminants dissolved or emulsified in the second liquid, comprises a first separation chamber which separates the immiscible liquids, a first discharge channel for discharging the first liquid into a housing, a mixing chamber for mixing the second liquid with a solvent, a second separation chamber for separating the second liquid from the solvent, and second and third discharge channels for discharging the solvent and second liquid, respectively, into the housing.

10 In accordance with a fourth aspect of the invention, a method of separating a mixture of first and second liquids into its component parts comprises injecting the mixture into a rotatable rotor, separating the first and second liquids from each other in a first separation chamber, discharging the first liquid from the rotor, injecting a solvent into the rotor, mixing the second liquid with the solvent, separating the second liquid from the solvent in a second separation chamber, discharging the solvent from the rotor, and discharging the second liquid from the rotor.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other objects, aspects, and embodiments of the present invention will be apparent to those skilled in the art from the following description and accompanying drawing figures, of which:

FIG. 1 is a partial elevational view in cross-section of an example of a single stage centrifugal separator according to the invention;

FIG. 2 is a partial elevational view in cross-section of the separator of FIG. 1 showing an alternative inlet port and vanes in the separation chamber;

FIG. 3 is a view along line 3-3 in FIG. 1;

FIG. 4 is a view along line 4-4 in FIG. 2;

FIG. 5 is a view along line 5-5 in FIG. 1;

FIG. 6 is an elevational view in cross-section of an example of a two stage centrifugal separator according to the invention.

5 DETAILED DESCRIPTION OF THE INVENTION

Referring first to FIG. 1, a single stage centrifugal separator 10 according to the invention separates a combined stream of two immiscible liquids of differing densities into its component parts. The invention will be described as separating a stream of oil mixed with water, though it will be understood that the invention efficiently separates other fluid combinations. The separator 10 comprises three principal components: a stationary shaft inlet port 12, a rotor 14 adapted for rotational movement around the inlet port 12, and a stationary housing shell 16 surrounding the rotor 14. The components comprise in construction a suitably rigid material such as steel or plastic in the preferred embodiment.

20 The oil and water mixture enters the separator 10 through a mouth 18 of the stationary shaft 12. This inlet arrangement has the advantage of eliminating contact of the mixture with the air between the rotor 14 and the housing 16, minimizing agitation and foaming which hamper separation. Additionally, the separator 10 can be used in any orientation as long as the output structures are appropriately designed since the oil/water mixture does not enter the space between the rotor 14 and the housing 16, and thus can not interfere with transfer of the separated liquids from the rotor to the housing. Nevertheless, the described embodiment of the separator 10 is intended for use in a vertical position with the fluid combination downwardly traveling through the inlet shaft 12, as shown by the arrows in FIG. 1.

35 The inlet shaft 12 comprises a single hollow shaft in the single-stage version or a plurality of smaller

shafts, such as a bundle of shafts or a concentric arrangement, which will be described later in conjunction with the two-stage embodiment of the invention.

5 The rotor 14 comprises a rotatable drive shaft 22, located coaxially to and beneath the inlet shaft 12, which is rotated by any suitable means such as a motor and accompanying drive train (not shown). The drive shaft 22 rotates the rotor at a speed determined to be
10 suitable in light of weir structure, relative densities of the fluids being separated, size of the separator components, magnitude of desired centrifugal force, and other factors familiar to those skilled in the art. If
15 desired, the drive shaft 22 may contain a drain channel 24, having a stopper or closure 26 secured therein by threading or other means, for convenient flushing and
20 draindown of the separator 10 by running a suitable cleansing fluid through the inlet port 12, allowing the fluid to run through the separator, and draining the
20 excess through the unstopped drain channel 24.

 A center wall 28 rises from the drive shaft 22, creating a mixing chamber 30 where the input fluid is mixed through shearing between the moving center wall 28
25 of the rotor and the outer wall of the stationary input shaft 12. The mixing chamber 30 has a small volume relative to, e.g., a mixing chamber at the periphery of a separator, minimizing shear resistance and thus the power required to maintain the rotor at the desired
30 speed. The volume of the mixing chamber optionally can be further decreased by mounting a frustoconical protrusion 32 on the stationary shaft 12 or by otherwise building up the volume displaced by the stationary shaft
35 12 or center wall 28. The mixing chamber may be optionally deleted where the mixing function is not needed as will be further described with reference to
FIG. 2. A primary purpose of the mixing chamber is for

addition of a conditioning material, such as a solvent for reducing viscosity or for solvent extraction.

The fluid mixture flows with the aid of externally applied pressure and centrifugal force from the mixing chamber, or optionally from the inlet shaft, into the separation chamber 34, formed by the center wall 28 and the coaxial outer wall 36, where the component fluids are separated. The outer wall 36 slopes oppositely from the center wall 28, causing the separated oil and water to move downwardly along the inner and outer walls, respectively, toward the separator's weir structures. The top of the outer wall 36 meets the stationary shaft 12 in annular engagement. At that location, bearings 38 are mounted between the wall 36 and the shaft 12 to enable the rotor 14 to rotate relative to the stationary shaft 12. Shaft seal 80 is provided to protect the bearing from contact with the internal fluids.

FIG. 2 illustrates an alternative inlet port 40 comprising a stationary shaft 42 which differs from the stationary shaft 12 in that it is shorter and capped by a disc 44 which extends out from the shaft 42 as a flange. The input fluid enters the rotor 14 through holes 46 near the bottom of the shaft 42 and in the disc 44. The center portion of the rotor 14 inside the center wall 28 and below the inlet port 40 is sealed off by a top wall 48, whereby the input fluid is shear mixed in the region between the disc 44 and the top wall 48 and the region between the disc 44 and the top of the outer wall 36 before entering the separation chamber 34. The inlet port 40 allows for complete flushing and draindown of the separator without a drain channel in the drive shaft 22, since no liquid collects in the region inside the center wall 28. Optionally, mixing of the input flow may be eliminated from the design of FIG. 2 by deleting the shear disk 44.

Referring again to FIG. 1, the oil and water of the input fluid combination separate in the separation

chamber 34 owing to the lighter density of oil relative to water. In the field of the centrifugal force created by the rotation of the rotor 14, the oil "rises" radially inwardly toward the center wall 28 while the water "sinks" radially outwardly toward the outer wall 36.

If desired, an optional sieve 50 illustrated in FIGS. 1 and 3 can be mounted between the center wall 28 and the outer wall 36 in the upper portion of the separation chamber 34 to aid the separation. The sieve 50 comprises a plurality of closely spaced, radially oriented plates parallel to the axis of rotation in the preferred embodiment. For oil/water separation, the plates are coated with or formed from a lipophyllic material such as polypropylene. While the fluid mixture travels through the sieve 50, finely dispersed or emulsified oil, which may be difficult to separate simply through centrifugal force, condenses on the surface of the plates and is thereby collected and separated from the water. Sieves used in gravitation separators have not been effective since they must be large with widely spaced plates in order to operate in a 1-g field. When used in the separator 10, however, the sieve can be small with closely spaced plates due to the higher magnitude of the g field. These modifications greatly improve separation effectiveness.

The sieve 50 also redirects and aligns the flow of incoming fluid. It has been found effective to guide the fluid in the axial direction to avoid shearing against the center and outer walls 28 and 36. Vanes or ribs 52, illustrated in FIGS. 2 and 4, may alternatively be mounted on the walls of the separation chamber to accomplish the same purpose. The vanes 52 may partially or completely traverse the separation chamber 34 in the radial direction.

As illustrated in FIGS. 1 and 5, the separation chamber 34 contains a weir 54 at its bottom for

direction of the separated oil and water. The weir 54 comprises an annular baffle plate attached to and extending from the drive shaft 22 toward the outer wall 36. The plate bends back upon itself to extend toward the center wall 28 before reaching the wall 36, at 54a, creating a segmented annular passage between the bend 54a and the outer wall 36 for the passage of water from the separation chamber 34. The weir plate ends a short distance from the center wall 28, creating an annular passage 58 between the edge of the weir 54 and the center wall 28 for the collection of oil from the separation chamber 34. The bent weir plate creates an intermediate oil collection chamber 59 under the top plate of the weir 54. The oil collected in the intermediate chamber 59 is shunted through a plurality of channels 61 formed through the bend 54a in the weir 54, the water passage 56, and the outer wall 36.

The outer wall 36 bends beneath and parallels the curvature of the weir 54 to shunt the collected water back toward the drive shaft 22. The outer wall 36 ends before contacting the drive shaft 22, thereby forming a second weir 60. An annular groove 62 is formed in the side of the outer wall 36 opposite the water passage 56 to receive wall 84 which divides the collection chambers 78 and 72 that respectively conduct outflows of water and oil. As illustrated in FIG. 1, the outer wall 36 is formed of an upper wall piece 36a and a lower wall piece 36b secured to each other by screws or other means. This component configuration is solely for convenience of construction. The wall 36 may if desired comprise a unitary piece without affecting separation. A sloped outcropping 64 extending from the drive shaft 22 guides water away from the shaft seal 82.

The outflow of separated fluids around the weir 54 is controlled so that a stationary oil/water interface is maintained between the outlets in the passages 56 and 58 during rotation. The interface must not approach

either outlet too closely or mixed fluid may be discharged. As in prior art apparatuses, air must be present adjacent the edges of each of the weirs 54 and 60 since separated liquid outflow rates are determined by free-surface flow over the weirs 54 and 60. In the present invention, however, the air/liquid interface at the center of the rotor 14 is largely eliminated by the radially outward slope of the center wall 28, which causes most of the center wall to be radially more outward than the edge of the weir 54, confining the necessary air/oil interface to a narrow pocket region adjacent the edge of the weir 54 where the center wall is sufficiently inward relative to the weir edge to establish a free liquid surface. Thus, the rotor 14 separates substantially all the input liquid without interaction with air and consequent foaming and interference with separation. A similar pocket of air is disposed near the edge of the weir 60. Air ducts 66 formed through the bottom plate of the weir 54 equalize pressure between the two pockets of air and remove excess gases therefrom which form, e.g., by bubbles of air mixed with the input fluid which "rise" to the center wall and migrate along it until they join with the pocket of air near the edge of the weir 54.

The sloping of the center and outer walls 28 and 36 allows the weirs 54 and 60 to be large in relation to overall rotor size, improving flow rate and separation efficiency. The formula for the position of the liquid/liquid (oil/water) interface between the separated liquids in the separation chamber 34 is

$$r_b = \sqrt{\frac{\rho_w r_w^2 - \rho_o r_o^2}{\rho_w - \rho_o}} \quad (1)$$

where

r_b is the radial distance of the liquid/liquid interface from the axis of rotation,
 5 r_w is the radial distance of the heavier liquid surface over the second weir edge,
 r_o is the radial distance of the lighter liquid surface over the first weir edge,
 10 P_w is the density of the heavier liquid, and
 P_o is the density of the lighter liquid.

15 The liquid/liquid interface in the separation chamber 34 must lie between the edge of the weir 54 and the bent portion 54a of the weir to avoid discharge of mixed fluid. This is expressed in mathematical terms as:

$$r_1 \leq r_b \leq r_p \quad (2)$$

20 where

r_p is the radial distance of the bent portion 54a of the first weir
 r_1 is the radial distance of the edge of the first weir.

25 Thus, as the distance between the edge of the first weir 54 and the bent portion 54a of the weir increases, the range of possible positions of the liquid interface increases and thus the range of liquid densities that
 30 can be separated by the weirs. These relationships can be used to design a weir structure that performs optimally for any particular application.

It has been found that the optimum weir construction for a separator designed to separate common
 35 crude oils from water where the crude oils have specific

gravities ranging from 0.82 to 0.92 satisfies the following relationship:

$$r_w = .937r_o + .05r_p + .008 \frac{r_p^2}{r_o} \quad (3)$$

The depth of the liquid over the edge of a weir, indirectly represented in the equations by r_w and r_o , depends on the relative proportions of the component fluids in the input mixture, viscosity, input flow rate, and speed of the rotor 14. The most effective designs will maintain a shallow flow over the weir edges. Air pressure at the weir edges must be equal in order for the above equations to be valid, accomplished by the air ducts 66 or other equivalent means.

The housing 16 collects the separated liquids from the rotor 14. The housing 16 is a single shaped wall which is formed around the rotor 14 and which completely encloses it. The annular top 68 of the housing, secured to the input shaft 12 by suitable means, extends out horizontally past the rotor 14. A sidewall 70 meets the edge of the top 68 and descends parallel to the outer wall 36 of the rotor. In the described embodiment the sidewall 70 is formed from two pieces 70a and 70b for convenience of construction, which are joined near the bottom of the sidewall 70 by screws or other suitable means in a fashion similar to the outer wall 36 of the rotor.

An oil collection chamber 72 is formed at the bottom of the sidewall 70 to receive the separated oil from the oil channels 61 through the wall 36. A water collection chamber 78 is formed adjacent to and radially inward from the oil collection chamber 72. An intermediate wall 84 is formed between the oil and water collection chambers 72 and 78 to keep the separated fluids apart. The end of the wall 84 fits into the annular groove 62 of the rotor to effectively prevent cross-contamination of the separated fluids. The collection chambers 72 and 78 are provided with attachments (not shown) for connection of pipes or hoses that remove the separated fluids.

The end of the radially inward wall 86 of the water collection chamber 78 fits against the drive shaft 22 underneath the outcropping 64 in annular engagement. Bearings 88 are mounted between the end of the wall 86 and the drive shaft 22 to allow the rotor 14 to rotate within the housing 16. A seal 82 is provided to protect the bearing from the internal fluids.

The separator 10 can be flushed and cleaned by operating it with a cleaning slurry containing water, pentane, and a suitable detergent, or another similar slurry formulation. The weirs and flow channels of the separator are sloped so that no liquid is trapped inside when the separator and the input liquid flow are stopped.

The separator 10 can be made in various sizes, all of which are functionally equivalent except that larger sizes will have a lower angular velocity in equivalent applications. The range of liquids that can be
5 separated remains the same.

FIG. 6 shows a two-stage separator 110 according to the invention. The separator 110 separates immiscible liquids containing dissolved contaminants or immiscible liquids that are resistant to separation, such as those
10 in an emulsion. The one-stage separator 10 is not able to separate out dissolved contaminants in mixed fluids in a single operation. The separator 10 is able to separate fluids resistant to separation to a degree, particularly with the help of the sieve 50, but does so
15 inefficiently. This is the case especially with very stable, finely dispersed colloidal suspensions and solutions.

As is known in the art, a separator such as the separator 10 can be used in two stages to separate
20 immiscible liquids and dissolved contaminants. The immiscible liquids first are separated through the process described above, and the separated liquid containing the contaminants is mixed with a solvent that has a higher affinity for the contaminants, by which
25 means the solvent breaks down the solution or emulsion and absorbs the dispersed contaminant into itself. The solvent and liquid, which preferably are immiscible, are then separated by putting them through the separator 10

a second time. The solvent can conveniently be mixed with the liquid containing the contaminant by putting them into the separator 10 in combination and allowing them to mix through the shear action in the mixing chamber 30 of separator 10 (FIG 1). If it is required that the liquid be of very high purity, the solvent purification process can be repeated until the desired level of purity is obtained.

Solvent extraction separation is desirable for mixtures such as commercial motor oil mixed with water, since commercial motor oils contain detergents that cause foaming and emulsions. A further example is a mixture of commercial gasoline with water: gasoline formulations contain carcinogenic substances as additives, such as benzene, toluene, ethyl benzene, xylenes, and naphthalene. The additives are slightly soluble in water, allowing a few parts per thousand to exist in solution.

The two-stage separator 110 carries out the required stages of initial separation, solvent extraction, and final separation in a single operation. The separator 110 will be described as separating motor oil mixed in water with the oil containing benzene contaminants which slightly dissolve in water. The solvent used is pentane. It will be understood that various other mixtures and solvents can be used. The separator 110 is similar in construction to the separator 10 in many aspects, except that, among other

differences, it contains two separation chambers with the high-density liquid output of the first chamber continuing into the second, radially more outward, chamber after being injected with a solvent.

5 The separator 110 comprises a stationary input shaft 112, a rotor 114, and a housing shell 116. The input shaft 112 comprises two coaxial shafts, an inner shaft 118 through which the oil/water mixture enters the separator, and an outer shaft 120 through which the
10 pentane solvent enters. The rotor 114 is driven by a rotatable drive shaft 122 under the power of a motor or other means (not shown). A drain channel 124 having a stopper 126 is provided in the drive shaft 122 for complete flushing and draindown of the separator 110.
15 The center wall 128 of the rotor 114 extends downwardly from its point of origin at the side of the mouth 130 of the inner input shaft 118, and slopes radially outwardly before ending near the top of the drive shaft 122. The center wall 128 is sealed from the outer input shaft 120
20 by an annular seal 132, preventing solvent from entering the chamber 134 formed by the center wall 128.

 An intermediate wall 136 attaches to the top of the rotatable shaft 122 and extends up and radially outward, creating a separation chamber 138 between the
25 intermediate wall 136 and the center wall 128. The input oil/water mixture enters the chamber 134 from the inner shaft 118 and is urged downwardly by external pressure and centrifugal force during rotation. The

mixture then flows around the edge of the center wall 128 into the separation chamber 138, wherein the separated components are urged upwardly by the radially outward slope of the intermediate wall 136 (for the water) and the radially inward slope of the center wall 128 (for the oil) toward a weir 140 disposed at the top of the separation chamber 138.

The weir 140 is similar in construction to the weir 54 in the single stage separator 10. The weir 140 comprises a baffle plate which originates from the center wall 128, extends radially outward, and bends back upon itself, creating an annular oil passage 142 between the edge of the weir 140 and the center wall 128. A water passage 144 is formed between the bent portion 140a of the weir and the intermediate wall 136, the latter curving around the weir 140 to continue the passage 144 and form a weir 146. For convenience of construction, the intermediate wall comprises two portions, a lower portion 136a and an upper portion 136b which are joined by welding or other suitable means near the bent portion 140a of the weir 140. An intermediate oil chamber 148 is formed in the interior of the weir 140, and an oil channel 150 is formed through the bent portion 140a of the weir, the water passage 144, and the intermediate wall 136.

The weirs in the two-stage separator 110 are preferably made in accordance with the optimal weir construction previously described.

The separation chamber 138 separates the oil/water mixture, after which the separated oil is directed through the passage 142, into the chamber 148, and through the channel 150. The water is directed into the passage 144 and over the edge of the weir 146. The air pockets over the weirs 140 and 146 communicate through air ducts 152, thereby equalizing their pressure.

An outer wall 156 is provided over the intermediate wall 136 to form an outer water passage 158 over the weir 146, and has air ducts 160 formed therethrough to allow the air pocket over the weir 146 to communicate with the housing space. The end of the outer wall 156 meets the input shaft 112 in annular engagement. Bearings 162 are mounted between the wall 156 and the shaft 112 to allow rotation of the rotor 114 around the input shaft 112. A seal 164 also is provided between the outer wall and the inlet shaft. A lip 166 is formed on the end of the center wall 128 at the point at which it meets the outer wall 156 in order to guide the water around the weir 146.

A solvent channel 168 is formed at the juncture of the outer wall 156 and the center wall 128 between the outer inlet shaft 120 and the outer water passage 158, supplying pentane solvent into the water stream just above the weir 146. The solvent and water mix in the outer passage 158 to remove emulsions and dissolved contaminants. The solvent channel 168 is directed so that the solvent is introduced into the high-velocity

water stream flowing over the weir 146 to facilitate mixing. The weir 146 is formed with an appropriate slope and contour to prevent the water flow from separating from the face of the weir, which facilitates
5 mixing and mitigates weir erosion. All weirs in the various illustrations are intended to illustrate similar slope and contour for this same purpose.

It can be seen that the oil channel 150 continues from the intermediate wall 136 through the outer water
10 passage 158 and outer wall 156 to a collection chamber in the housing 116.

The outer water passage 158 continues down between the intermediate wall 136 and outer wall 156 until it enters a second separation chamber 170 formed between
15 the walls 136 and 156. The separation chamber 170 separates the water from the solvent, which contains the extracted contaminants. The outer wall 156 slopes radially outward to urge the cleaned and separated water down to a weir 172 formed at the bottom of the
20 separation chamber 170 which directs the separated liquids out of the separation chamber 170. Pentane has lesser density than water, so the pentane "rises" radially inward toward and is urged downward by the radially inwardly-sloped intermediate wall 136 while the
25 water "sinks" radially outward against the outer wall 156.

The weir 172 is formed from a baffle plate originating on the drive shaft 122, extending radially

outward, bending back on itself, and ending before reaching the drive shaft 122 forming an annular solvent passage 174. A water passage 176 is formed between the bent portion 172a of the weir and the outer wall 156, which curves under the weir 172 and ends to form a weir 178. A solvent channel 180 is formed through the bent portion 172a, passage 176, and outer wall 156 to shunt the collected solvent into the housing 116.

The outer wall 156 is formed from three secured pieces 156a, 156b, and 156c for convenience of construction. An annular groove 181 is formed on the outer side of the lower section 156c.

An outcropping 182 extends from the bottom of the weir 172 around the edge of the weir 178 to guide the water into the housing 116. A small air channel 184 underneath the outcropping 182 leads from the housing air space to a cavity 186. Air ducts 188 lead from the cavity 186 to the air pocket at the edge of the weir 172 to equalize the pressure therein.

The housing 116 comprises a top wall 190 secured in annular attachment to the inlet shaft 112 by welding or other means. The top wall 190 extends horizontally outward over the outer wall 156 of the rotor 114, and a side wall descends from it to form an oil collection chamber 192 below the oil channel 150. The chamber 192 receives and collects the separated oil. An attachment (not shown) to the chamber 192 affords connection to a pipe or hose for discharge of the separated oil.

The radially inward wall 198 of the oil collection chamber 192 descends substantially parallel to the outer wall 156 of the rotor, and forms a solvent collection chamber 200 below the solvent channel 180 for the collection of solvent and accompanying contaminants. An attachment (not shown) to the solvent collection chamber 200 affords connection to a pipe or hose for discharge of the solvent. The discharged solvent may be recycled and reused in the separator 110, if desired.

10 The inner wall 206 of the solvent collection chamber 200 ends inside the annular groove 181 to effectively prevent cross-contamination with purified water in chamber 208. The wall 206 also serves as the outer wall of the water collection chamber 208 formed
15 beneath the weir 178 for collection of water which has been separated from the oil and additionally purified of benzene or other impurities. In other words, the purified water contains neither immiscibles nor solubles. An attachment (not shown) to the water
20 collection chamber is provided for connection of a pipe or hose for removal of the purified water.

The inner wall 210 of the water collection chamber ends in annular engagement with the drive shaft 122. Bearings 212 are mounted between the wall 210 and the
25 drive shaft 122 to allow the drive shaft to rotate within the housing. An annular seal 204 is placed adjaced to bearings 212 to protect them from the internal fluids.

One run through the separator 110 is sufficient to separate out immiscibles and solubles from the water. If desired, the operation can be repeated in order to achieve a higher level of purity.

5 It will be understood that many different combinations of liquids can be separated by the separator 110. It will also be understood that the different auxiliary structures described with regard to the separator 10 such as the sieve 50 and vanes 52 can
10 also be used beneficially in the separator 110. The present invention includes modifications and variations of the described embodiments, which constitute only a few examples of how the invention may be applied in practice.

CLAIMS

1. Apparatus for centrifugally separating into
5 its component parts a mixture having immiscible
component parts of a first liquid and a second liquid of
differing densities, comprising:

an elongate hollow inlet shaft having an open
receiving end for receiving the mixture and an open
10 discharge end through which the mixture is delivered
into the apparatus;

a rotor rotatably disposed substantially coaxially
to and surrounding the inlet shaft, said rotor including
reception means for receiving mixture from the inlet
15 shaft, separation means receiving mixture from the
reception means for separating mixture into its
component liquid parts automatically without need for
external control or adjustment, and discharge means for
discharging the separated liquids of the mixture from
20 the rotor;

rotation means for rotating the rotor around the
inlet shaft;

a housing surrounding the rotor for receiving and
collecting the separated liquids from the rotor.

25

2. The apparatus of claim 1 further comprising a
second inlet shaft disposed coaxially to the inlet
shaft.

3. The apparatus of claim 1 wherein the reception means comprises a substantially circular wall perpendicular to the inlet shaft and spaced from the discharge end thereof and a frustoconical center wall angularly attached to the circular wall and extending therefrom toward the inlet shaft and past the discharge end thereof, sloping radially outward, thereby surrounding a portion of the inlet shaft and forming a mixing chamber between the inlet shaft and the center wall.

4. The apparatus of claim 3 wherein the inlet shaft is substantially cylindrical and further comprising a frustoconical attachment to the inlet shaft having approximately the same radial slope as the center wall.

5. The apparatus of claim 1 wherein the separation means comprises an elongate annular separation chamber with the inlet shaft at the approximate center of the annulus, the separation chamber having an annular inlet end for input of the mixture from the rotor reception means, an annular discharge end located oppositely from the inlet end, a first weir being disposed at the discharge end, an elongate annular inner wall having a radially inward slope from the inlet end to the discharge end, and an

elongate annular outer wall having a radially outward slope from the inlet end to the discharge end.

6. The apparatus of claim 1 wherein the
5 separation means comprises an elongate annular separation chamber with the inlet shaft at the approximate center of the annulus, the separation chamber having an annular inlet end for input of the mixture from the rotor reception means, an elongate
10 annular inner wall, an elongate annular outer wall, and an annular discharge end at which is disposed a first weir attached to the center wall extending radially outward toward the outer wall, bending back upon itself in the direction of the inlet end before contacting the
15 outer wall, and extending radially inward after the bend toward the inner wall but ending at an annular edge before contacting the inner wall, forming a heavier liquid passage between the first weir and the outer wall, and a lighter liquid passage between the edge of
20 the weir and the inner wall, and further comprising a lighter liquid channel formed through the weir at approximately the bend thereof, through the heavier liquid passage, and through the outer wall.

25 7. The apparatus of claim 6 wherein the outer wall curves under the first weir in an approximately radially inward direction, lengthening the heavier liquid passage, and further comprising an elongate

annular opposing wall disposed radially inward of the heavier liquid passage, and wherein the outer wall ends in an annular edge which is spaced from the opposing wall, thereby forming a second weir.

5

8. The apparatus of claim 7 further comprising means for communication of air pressure between the lighter liquid passage and the heavier liquid passage.

10

9. The apparatus of claim 7 wherein the opposing wall forms an outcropping approximately opposite the edge of the second weir.

15

10. The apparatus of claim 1 wherein the rotation means comprises a drive shaft disposed substantially coaxially to the inlet shaft and axially spaced therefrom, and further comprising a drain channel formed in the drive shaft.

20

11. The apparatus of claim 1 wherein the inlet shaft is substantially cylindrical and wherein the rotor comprises an annular elongate outer wall surrounding the inlet shaft, one edge of the outer wall being rotatably connected to and sealed against the inlet shaft.

25

12. The apparatus of claim 6 wherein the edge of the first weir is disposed farther radially inward than a portion of the inner wall.

13. The apparatus of claim 6 further comprising a plurality of closely-spaced substantially radially disposed plates mounted between the inner wall and the
5 outer wall of the separation chamber.

14. The apparatus of claim 13 wherein the mixture comprises oil and the plates comprise a lipophilic material.

10

15. The apparatus of claim 6 further comprising a plurality of vanes mounted to the inner or outer walls of the separation chamber extending radially into the separation chamber.

15

16. The apparatus of claim 7 wherein the apparatus satisfies the following relationship when used to separate hydrocarbons having specific gravities ranging from 0.82 to 0.92 from water:

$$r_w = .937r_o + .05r_p + .008 \frac{r_p^2}{r_o}$$

20

17. The apparatus of claim 7 wherein the housing comprises an elongate annular housing wall secured at its top to the inlet shaft, a lighter liquid collection chamber disposed adjacent the lighter liquid channel,
25 and a heavier liquid collection chamber disposed adjacent the second weir, and wherein the rotation means

comprises a rotatable drive shaft in rotatable annular engagement with the housing, and further comprising an annular groove formed in the radially outward surface of the outer wall which engages a portion of the housing wall.

18. A method of centrifugally separating a mixture having component parts of first and second immiscible liquids comprising the steps of:

10 supplying the mixture through an inlet shaft into the approximate center of a rotatable rotor having a radially outwardly sloping center wall with an annular outer edge surrounding the input shaft;

rotating the rotor, causing the mixture to move
15 down the slope of the center wall and flow over the edge thereof into a separation chamber formed by the center wall and a coaxial outer wall having an opposite radial slope from the center wall and a first weir disposed oppositely from the center wall edge;

20 separating the mixture into its component parts in the separation chamber;

discharging the first liquid from the separation chamber through a first annular channel between the center wall and the first weir;

25 channeling the first liquid to a first collection chamber;

discharging the second liquid from the separation chamber through a second annular channel between the outer wall and the first weir;

channeling the second liquid to and over a second
5 weir and into a second collection chamber;

19. The method of claim 18 further comprising the step of equalizing air pressure over the first and second weirs.

10

20. The method of claim 18 further comprising the step of engaging a groove formed in the outer wall with a wall formed between the first and second collection chambers.

15

21. The method of claim 18 further comprising the step of directing the mixture through a plurality of closely spaced plates in the separation chamber.

20

22. An apparatus for centrifugally separating into its component parts through solvent extraction or other chemical means a liquid mixture having first and second immiscible liquids and contaminants dissolved or emulsified in the second liquid, comprising:

25

an elongate hollow inlet shaft including a first receiving end for receiving mixture, a second receiving end for receiving a solvent, a first discharge end through which the mixture is input into the apparatus,

and a second discharge end through which the solvent is delivered into the apparatus;

a rotor rotatably disposed substantially coaxially to and surrounding the inlet shaft, said rotor including
5 first reception means for receiving the mixture from the inlet shaft, first separation means for separating the mixture into its immiscible liquid parts, first discharge means for discharging the separated first liquid from the rotor, second reception means in the
10 rotor for receiving the solvent from the input shaft, mixing means for mixing the solvent with the second liquid whereby the solvent at least partially absorbs the contaminants, second separation means for separating the solvent and absorbed contaminants from the second
15 liquid, second discharge means in the rotor for discharging the separated second liquid from the rotor, and third discharge means in the rotor for discharging the separated solvent from the rotor;

rotation means for rotating the rotor around the
20 inlet shaft;

a housing containing first, second, and third collection chambers for receiving and collecting the first liquid, second liquid, and solvent from their respective discharge means.

25

23. The apparatus of claim 22 wherein the first separation means comprises a first elongate annular separation chamber having an annular inlet end, a first

inner wall sloped radially inward from the inlet end, a first outer wall sloped radially outward from the inlet end, a first weir disposed oppositely the inlet end, a lighter liquid annular passage formed between the first
5 weir and the first inner wall, and a heavier liquid annular passage formed between the first weir and the first outer wall

24. The apparatus of claim 23 wherein the first
10 outer wall bends underneath the first weir radially inward and ends, lengthening the heavier liquid passage and forming a second weir, and wherein the solvent is injected from the second discharge end of the inlet port near the edge of the second weir.

15

25. The apparatus of claim 24 further comprising an air duct disposed between the first and second weirs to equalize pressure therein.

20 26. The apparatus of claim 22 wherein the second separation means comprises a second annular elongate separation chamber disposed radially outward from the first separation means.

25 27. A method of separating a mixture of first and second liquids into its component parts comprising:

injecting the mixture into a rotatable rotor;

separating the first and second liquids from each other in a first separation chamber;

discharging the first liquid from the rotor;

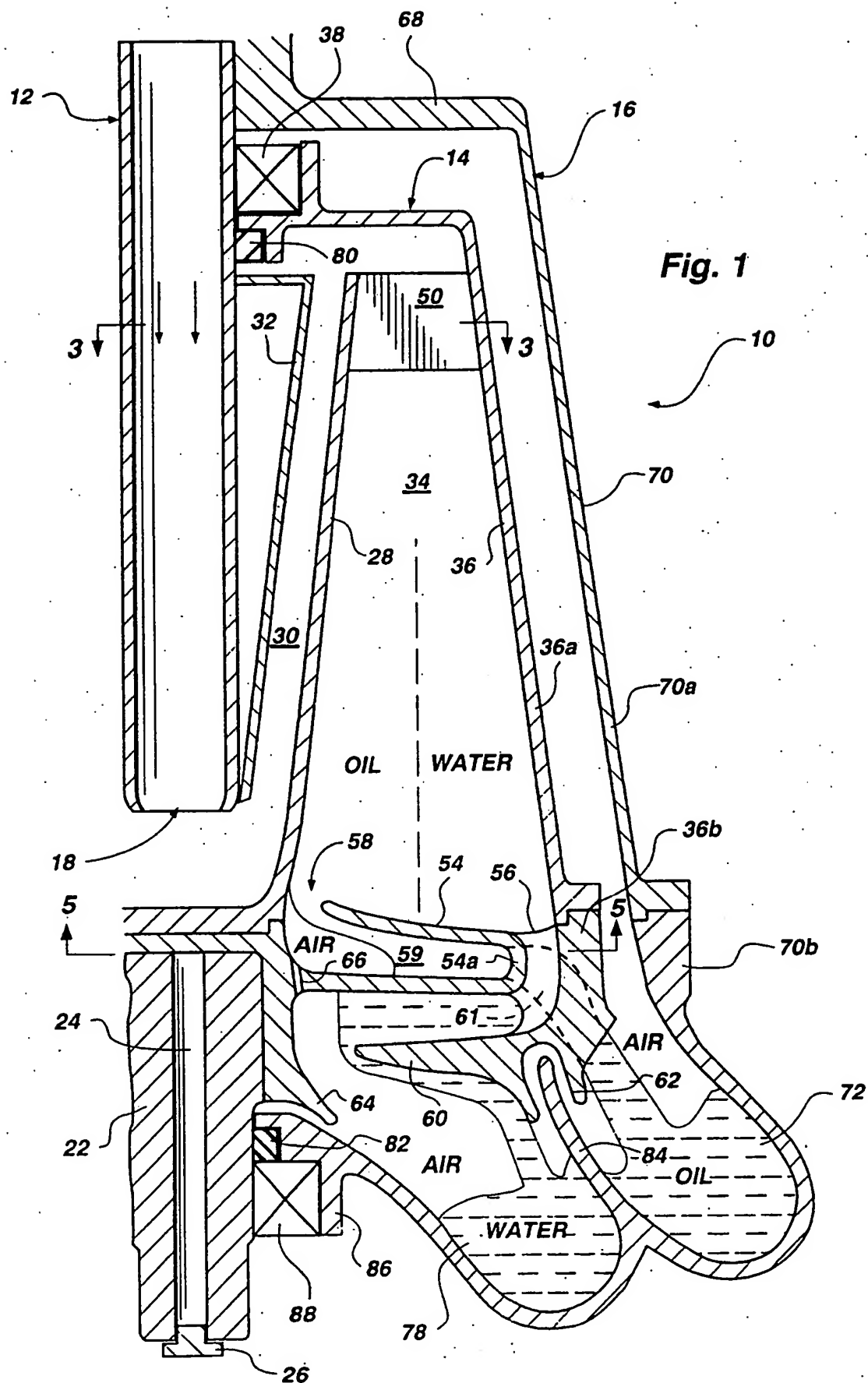
injecting a solvent into the rotor;

5 mixing the second liquid with the solvent;

separating the second liquid from the solvent in a second separation chamber;

discharging the second liquid from the rotor;

discharging the solvent from the rotor.



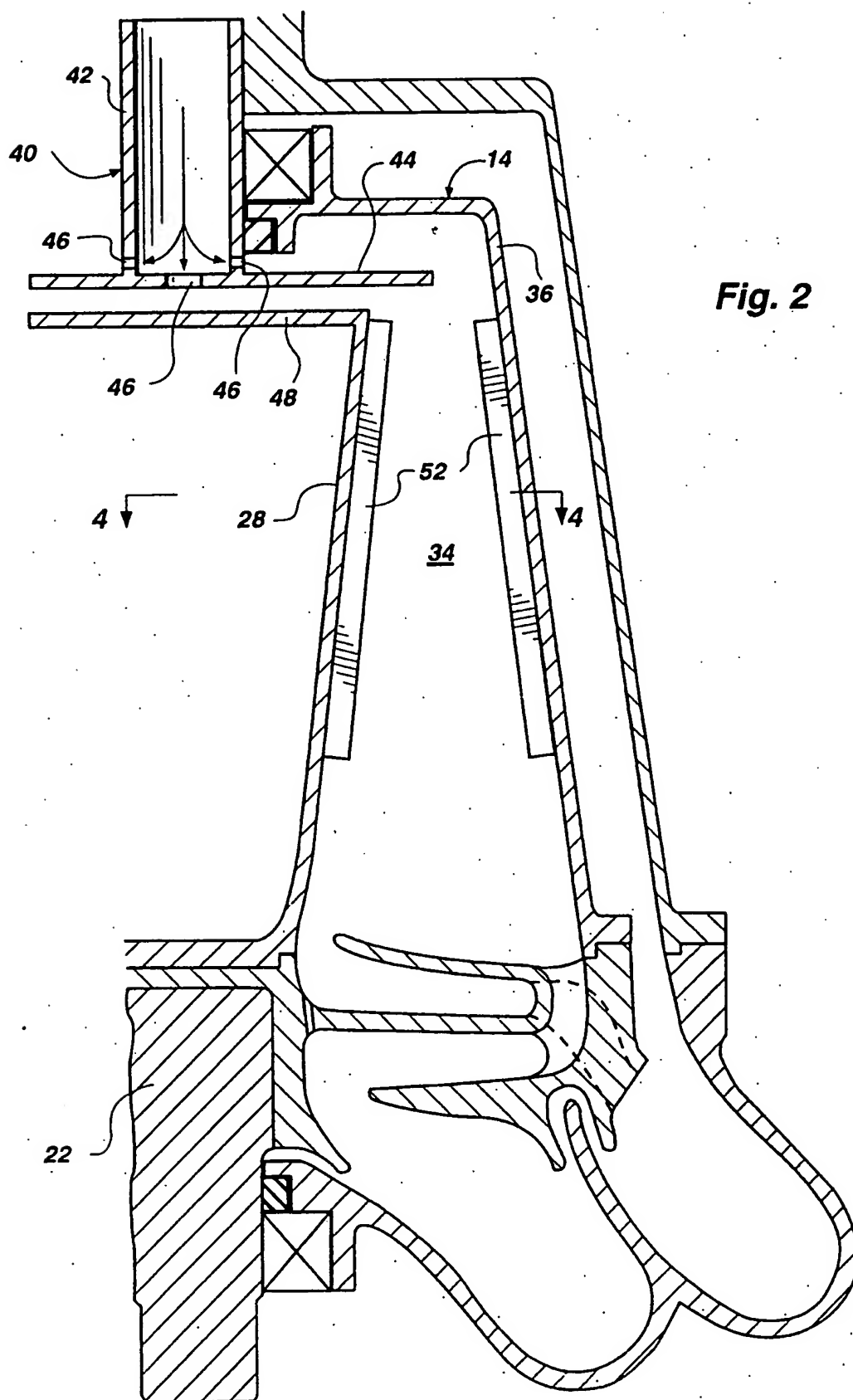


Fig. 3

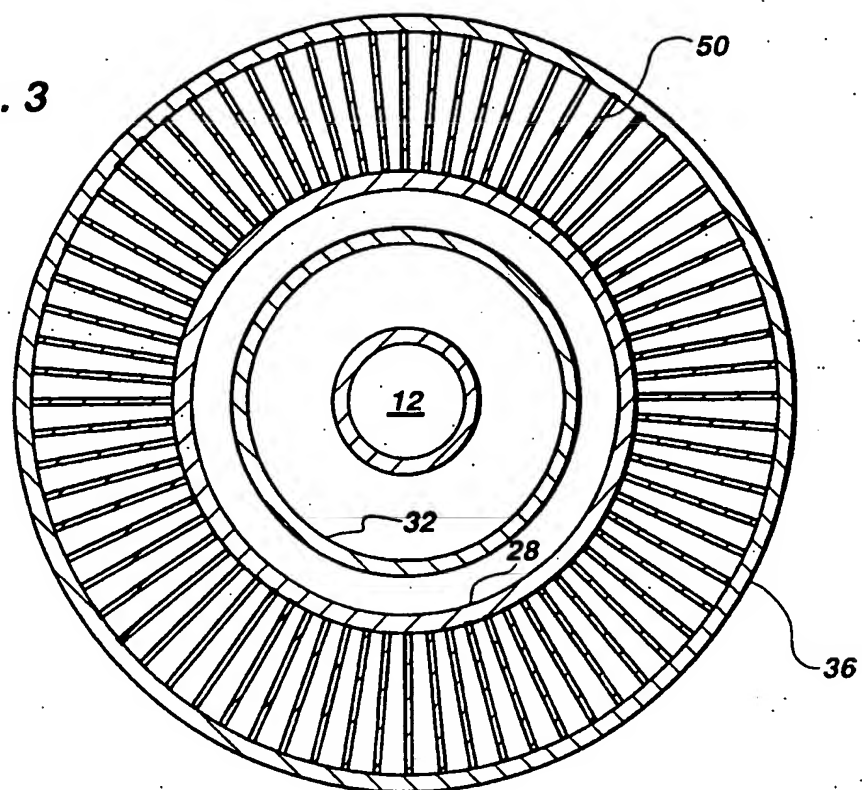


Fig. 4

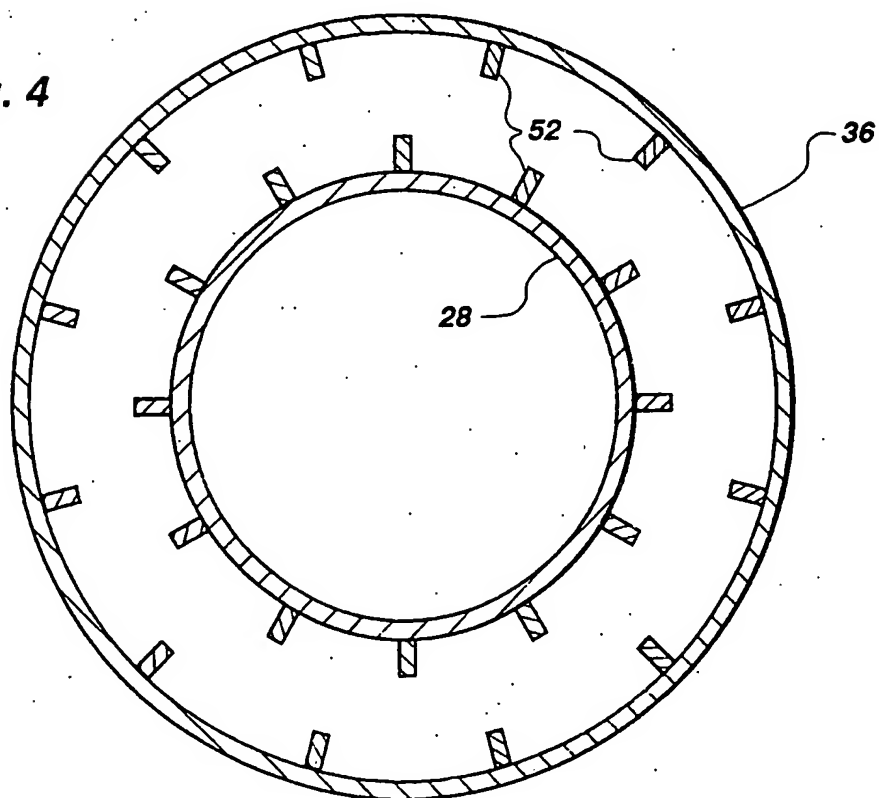
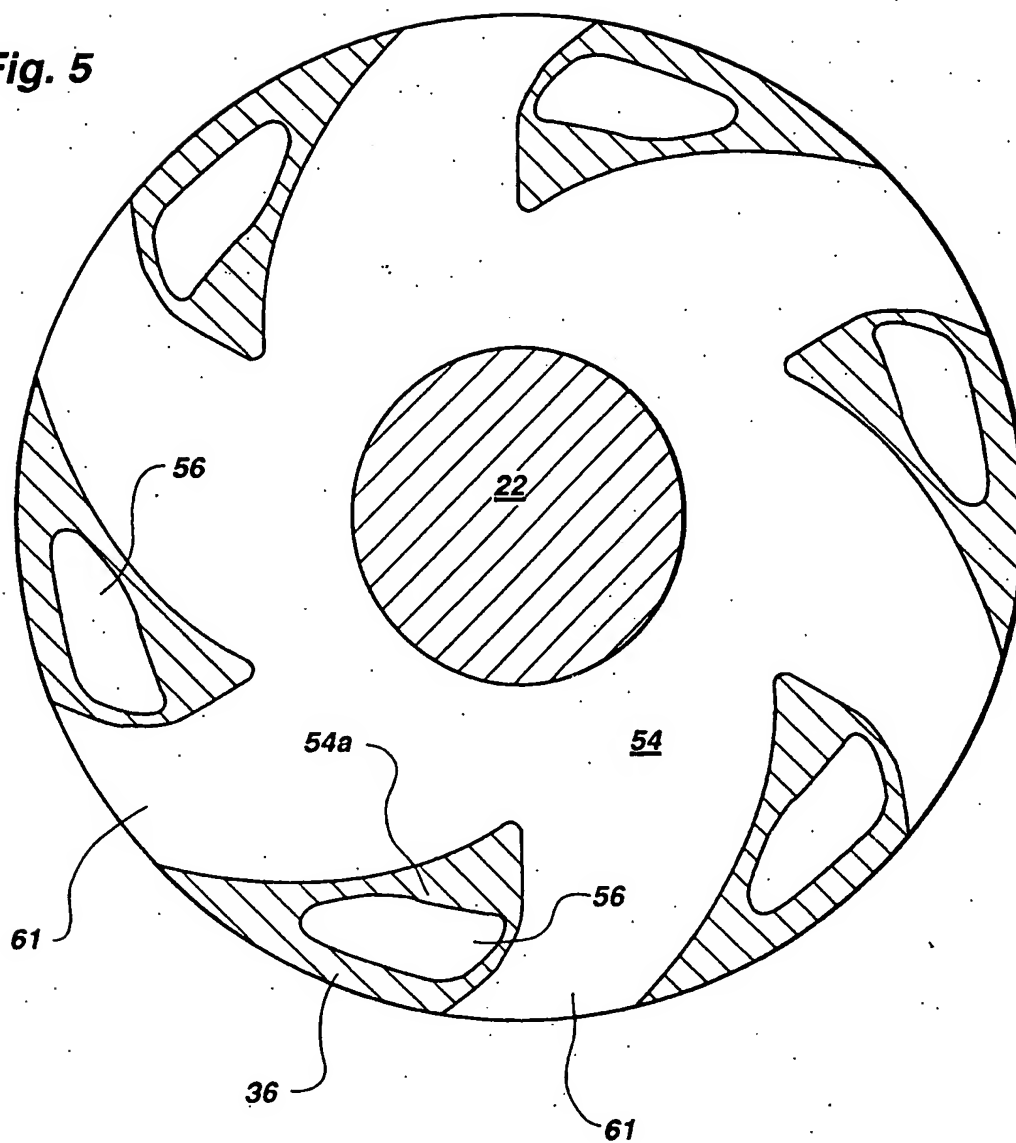
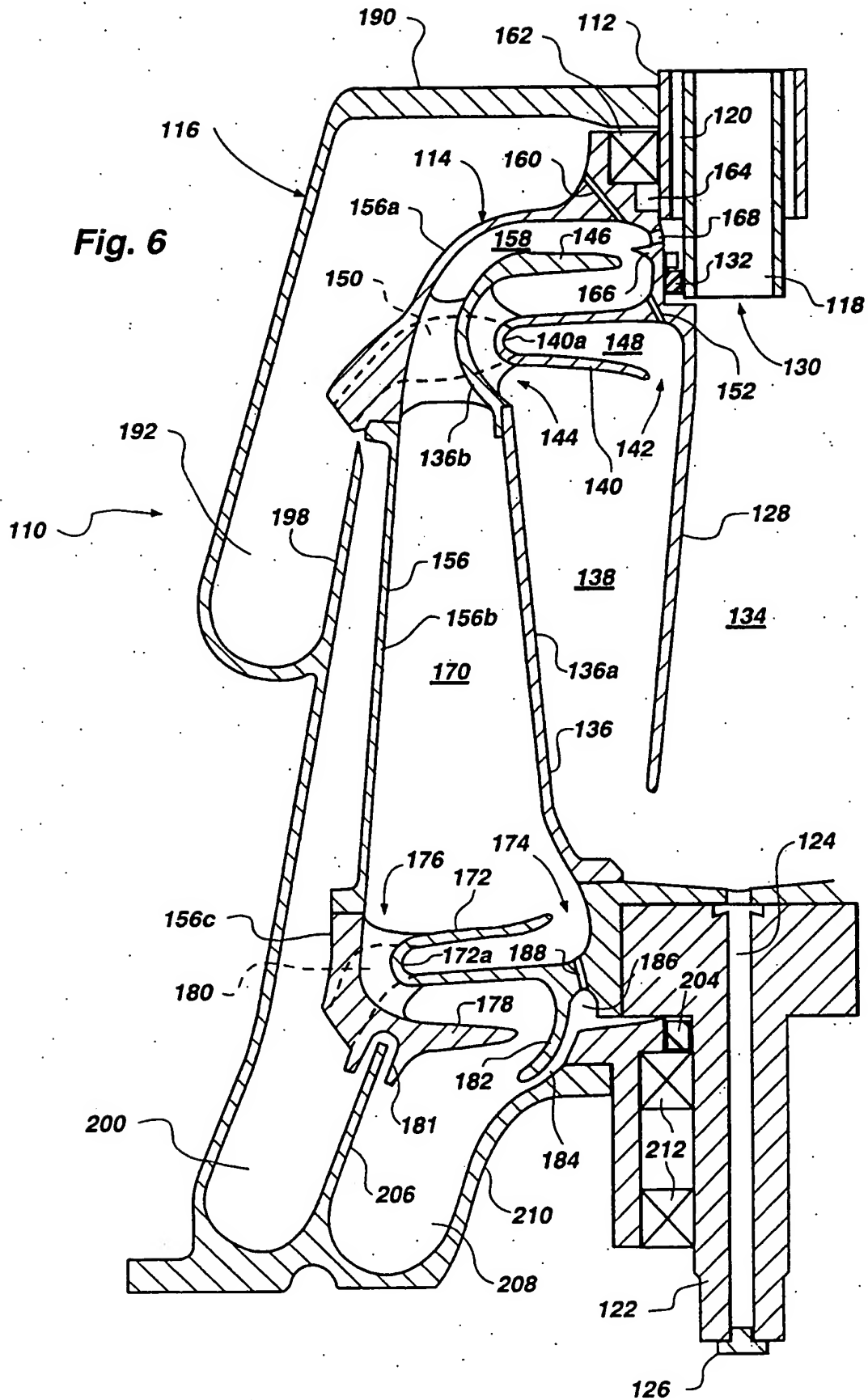


Fig. 5





INTERNATIONAL SEARCH REPORT

International application No.

PCT/US93/05505

A. CLASSIFICATION OF SUBJECT MATTER

IPC(5) :B01D 21/26

US CL :210/360.1, 380.1, 787; 494/17, 37, 43, 60

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 210/360.1, 380.1, 787; 494/43, 60

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X,P -- Y,P	US, A, 4,069,123 (Lavin) 22 September 1992, Abstract.	1, 5, 10 ----- 2
Y	US, A, 4,959,158 (Meikrantz) 25 September 1990, Col. 2, line 40.	2
X	US, A, 4,190,530 (Forsythe, Jr. et al.) 26 February 1980, Abstract, lines 1-10	27

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
A document defining the general state of the art which is not considered to be part of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
E earlier document published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means	
P document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

21 SEPTEMBER 1993

Date of mailing of the international search report

OCT 04 1993

Name and mailing address of the ISA/US
Commissioner of Patents and Trademarks
Box PCT
Washington, D.C. 20231

Facsimile No. NOT APPLICABLE

Authorized officer

ROBERT DAWSON

Telephone No. (703) 308-0456

**This Page is Inserted by IFW Indexing and Scanning
Operations and is not part of the Official Record**

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ BLACK BORDERS
- ☐ IMAGE CUT OFF AT TOP, BOTTOM OR SIDES
- ☒ FADED TEXT OR DRAWING
- ☒ BLURRED OR ILLEGIBLE TEXT OR DRAWING
- ☐ SKEWED/SLANTED IMAGES
- ☐ COLOR OR BLACK AND WHITE PHOTOGRAPHS
- ☐ GRAY SCALE DOCUMENTS
- ☐ LINES OR MARKS ON ORIGINAL DOCUMENT
- ☒ REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY
- ☐ OTHER: _____

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.